



# Exterior Non-Ductile Beam-Column Joints

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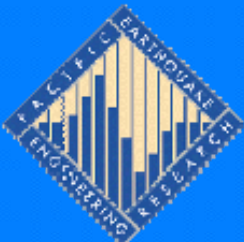
under the guidance of

**Professor Moehle**

University of California, Berkeley

**SangJoon Park**

University of California, Berkeley



August 13th 2008

# Background

*Background*

Specimen  
Specifications

Shear Capacity  
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- Many Reinforced Concrete buildings in Los Angeles built prior to the adaptation of modern seismic codes were designed with insufficient lateral capacity
  - Most classified as being insufficient
    - Susceptible to collapse
  - Current guidelines are too conservative
    - Retrofit costs high
- **Objective:** To research exterior non-ductile beam-column joints experiencing early column failure



# Specimen Specifications

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*Specimen Specifications*

Shear Capacity Calculations

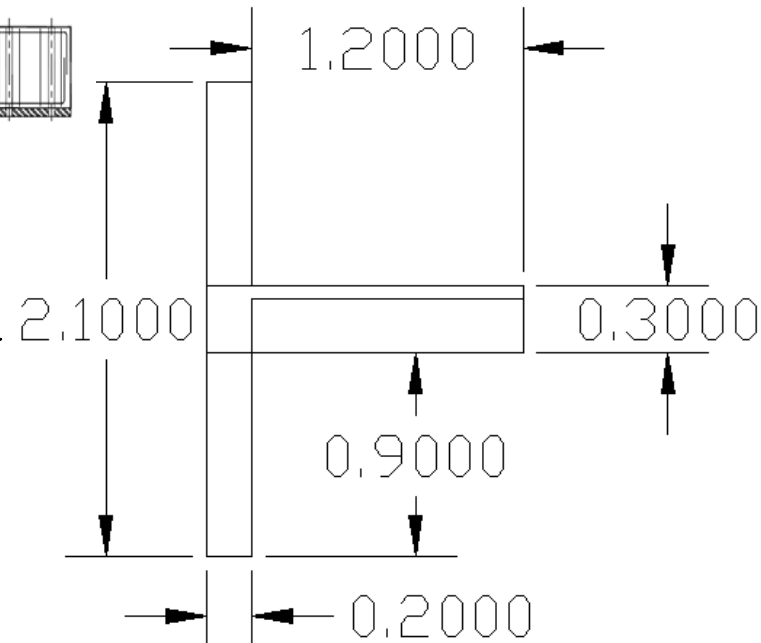
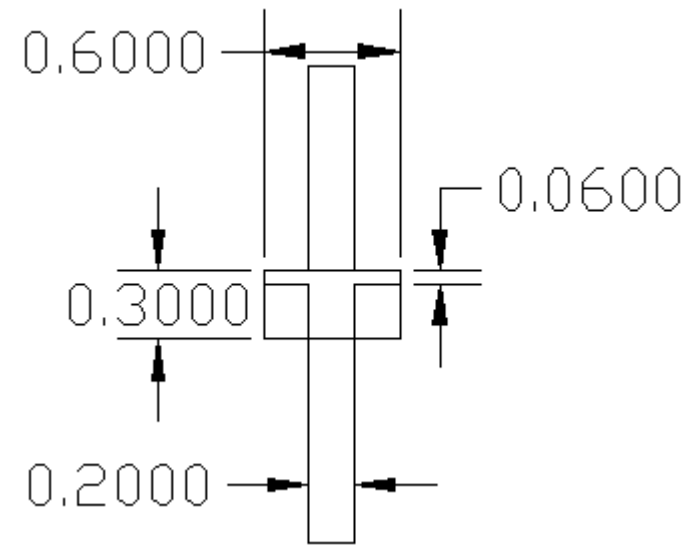
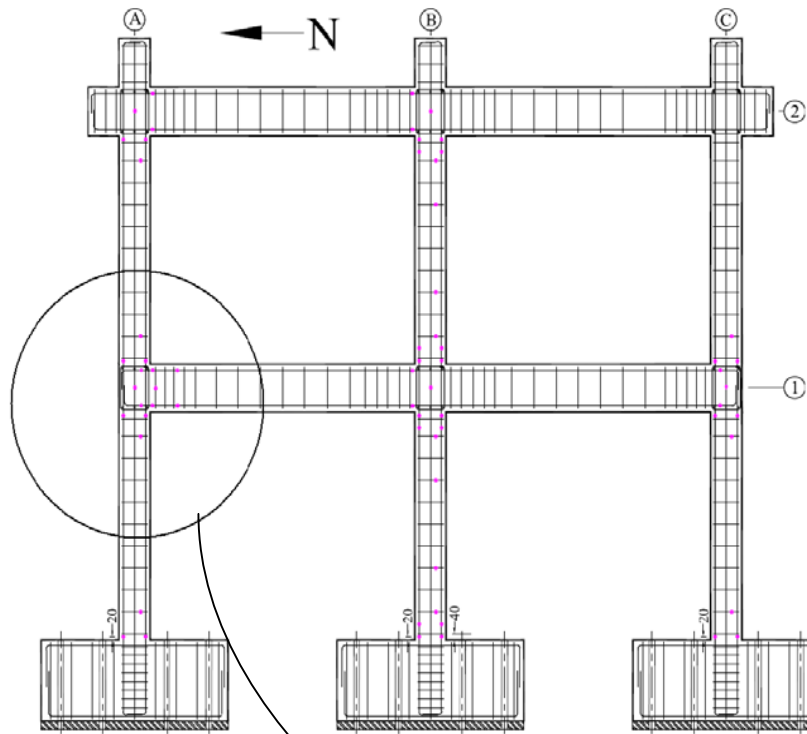
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# Specimen Specifications

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**Specimen 1:**

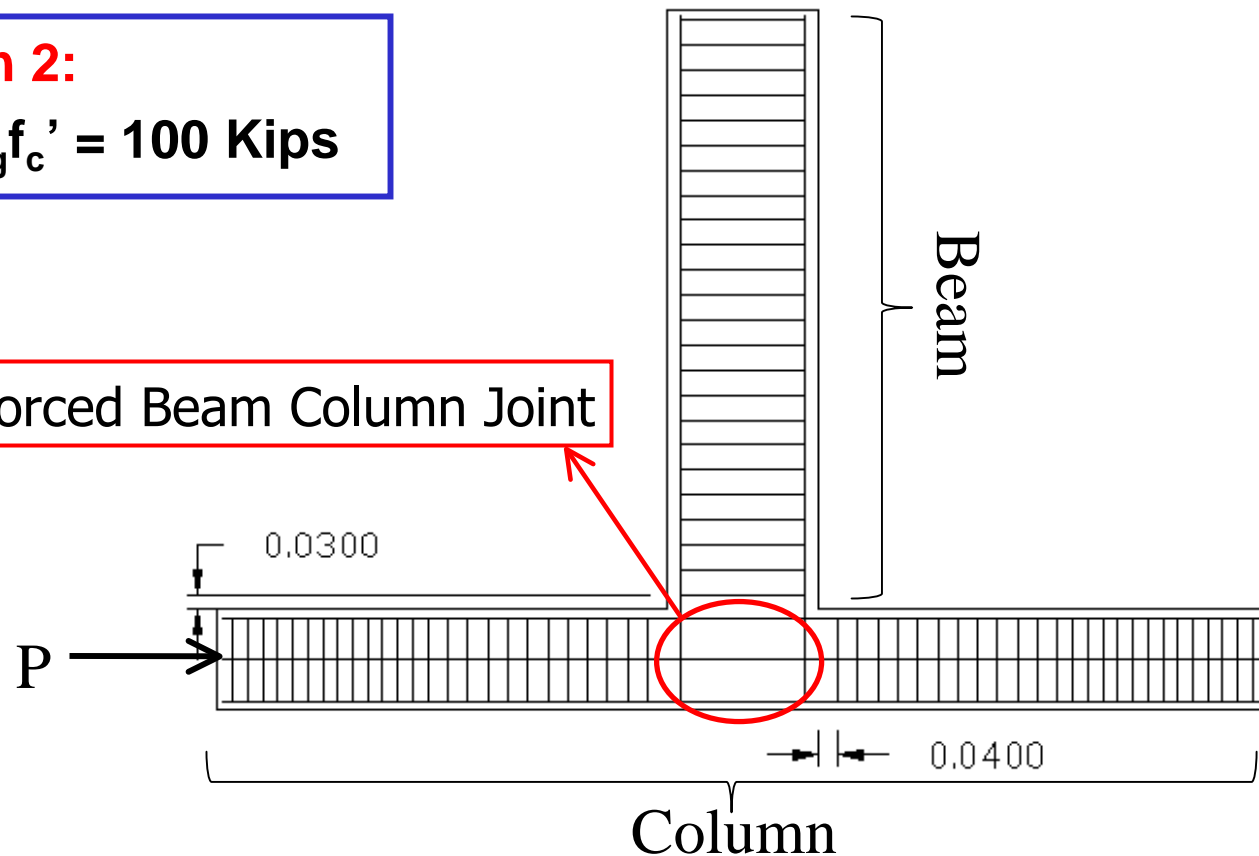
$$P = 0.2 A_g f_c' = 50 \text{ Kips}$$

**Specimen 2:**

$$P = 0.4 A_g f_c' = 100 \text{ Kips}$$

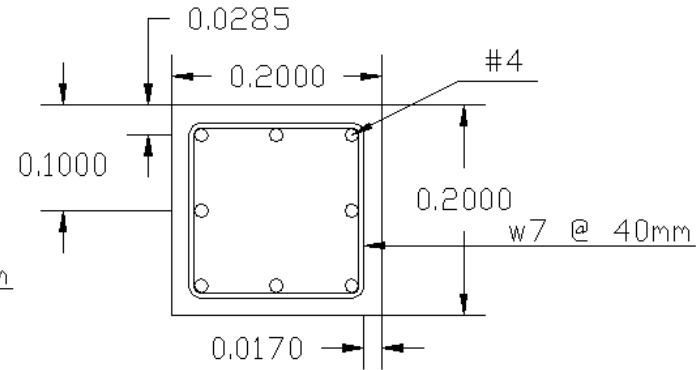
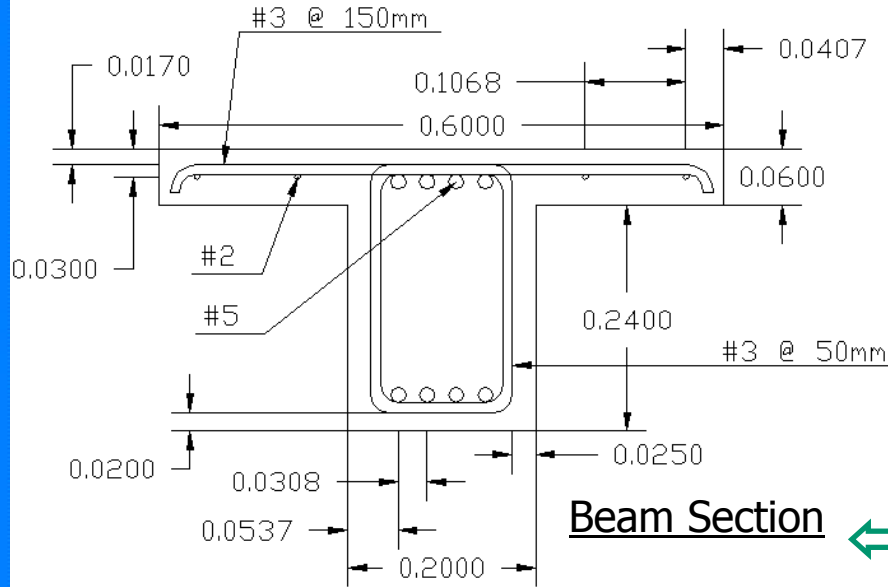
Hoops and Stirrups

Unreinforced Beam Column Joint



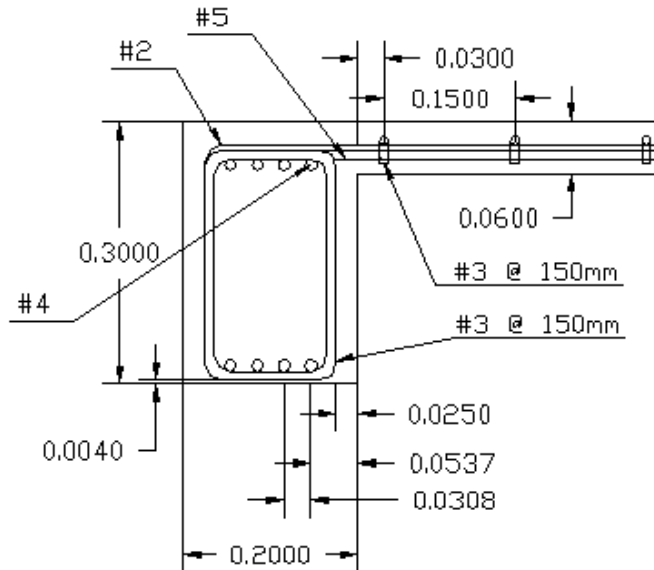
# Specimen Specifications

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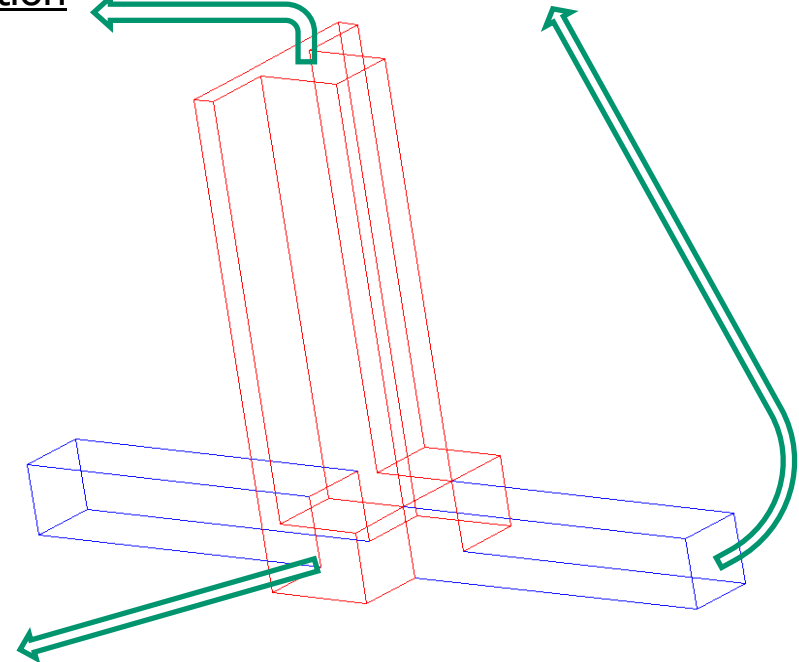


Beam Section

Column Section



Transverse Beam Section



# Specimen Specifications

Material properties used in analyses

$$f'_c = 4 \text{ Ksi}$$

Steel Bar	$F_y$ (Ksi)	$\epsilon_y$	$F_u$ (Ksi)	$\epsilon_u$
5mm (smooth)	95.29	0.005	99.50	0.02
#2 (deformed)	33.61	0.002	51.20	0.12
#3 (deformed)	60.00	0.008	90.00	0.09
#4 (deformed)	70.00	0.005	100.0	0.12
#5 (deformed)	70.00	0.005	100.0	0.12
#6 (deformed)	70.00	0.005	100.0	0.12

Real material properties

Steel Bar	$F_y$ (Ksi)			$\epsilon_y$ (%)	$F_u$ (Ksi)			$\epsilon_u$ (%)
	max	average	min		max	average	min	
w 7		88.80		0.7		107.1		2.237
#2 (w 5)	64.35	63.45	62.96	0.474	75.26	74.08	72.67	17.88
#3	65.33	65.27	65.23	0.436	105.1	104.8	104.6	11.86
#4	65.92	67.76	71.37	0.460	104.5	96.25	91.36	12.21
#5	67.00	66.60	66.33	0.521	90.43	90.1	90.12	12.5

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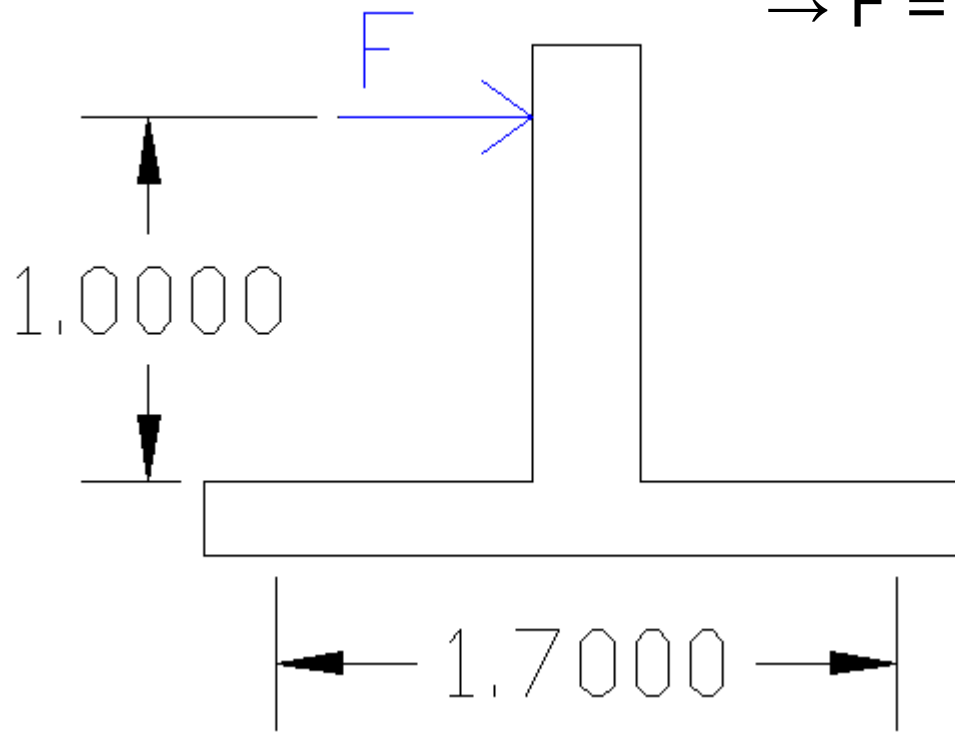


# Shear Capacity Calculations

→ Column failure

Balanced moment failure of the column : 438.6 k-in

→  $F = 22.3$  kips



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# Shear Capacity Calculations

$\gamma$  = Joint Shear Strength Factor

Specimen 1 (50 Kips) :

- Column

\* Yielding :  $M=412$  k-in  $\rightarrow F=20.9$  Kips }  $\gamma = 12.92$  (psi)

\* Failure :  $M=412$  k-in  $\rightarrow F=20.9$  Kips }

Specimen 2 (100 Kips):

- Column

\*Yielding :  $438.6$  k-in  $\rightarrow F=22.3$  Kips  $\rightarrow \gamma = 13.79$  (psi)

\*Failure :  $427.1$  k-in  $\rightarrow F=22.2$  Kips  $\rightarrow \gamma = 13.74$  (psi)

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# Cage

## *Beam*

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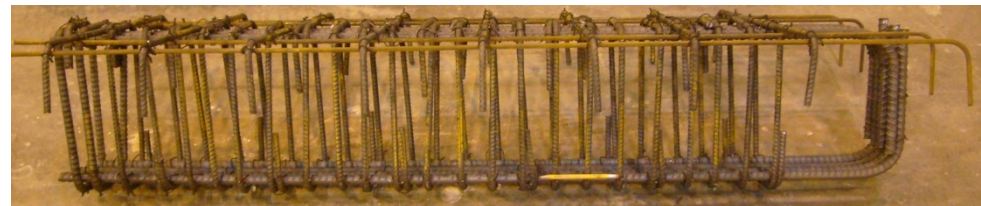
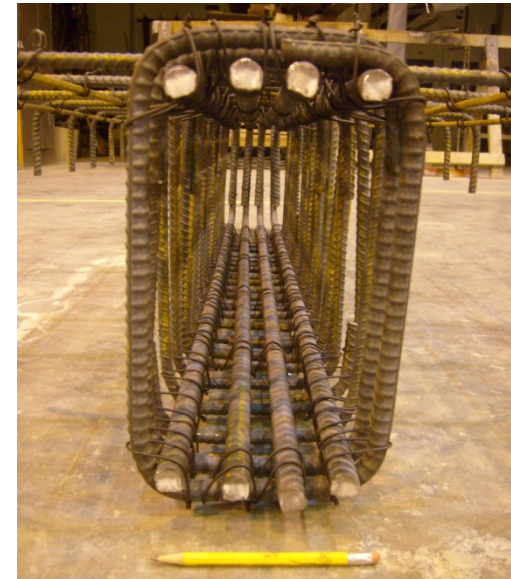
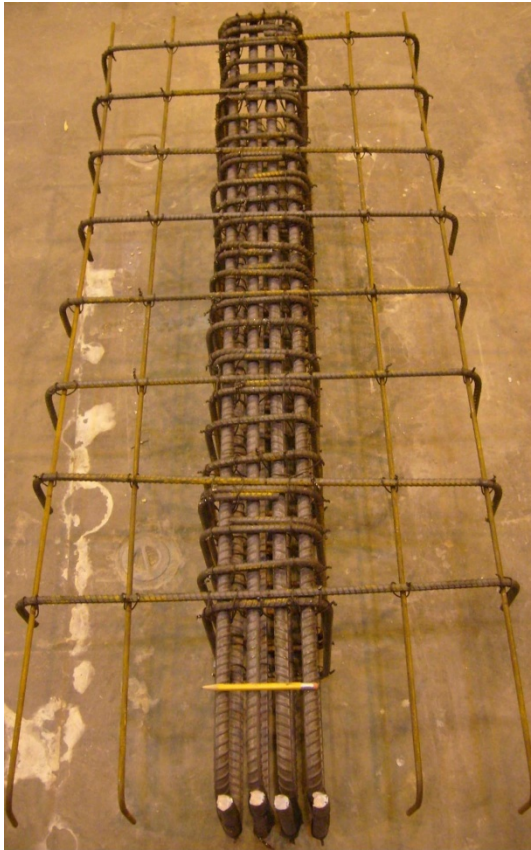
*Cage*

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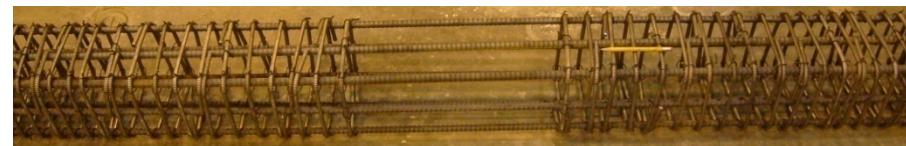
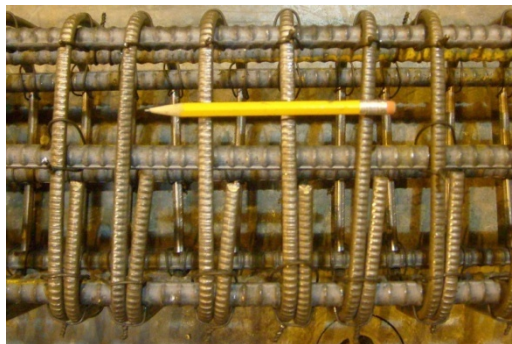
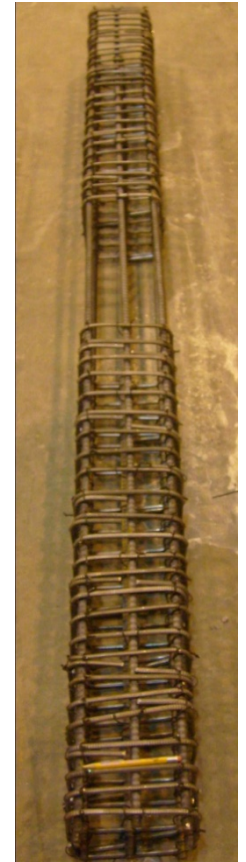
Testing



# Cage

## *Column*

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# Form

## *Beam*

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# Form

## *Beam*

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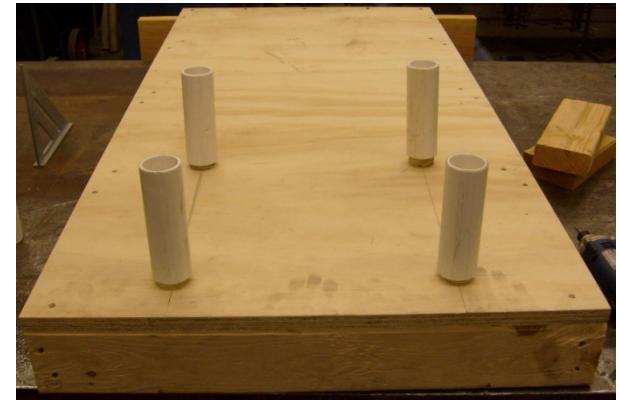
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# Form

## *Column*

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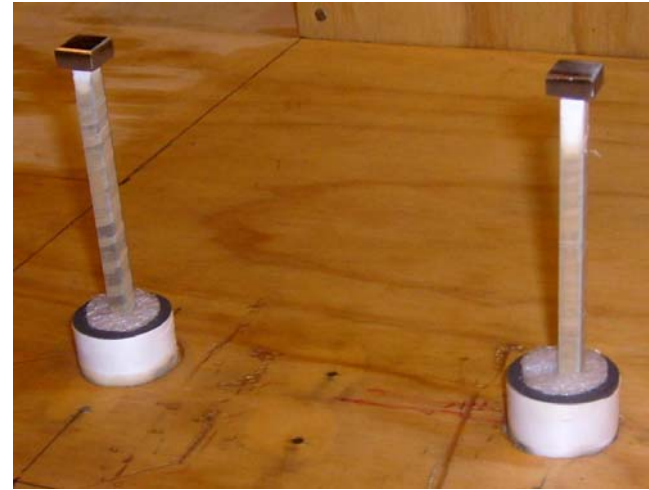
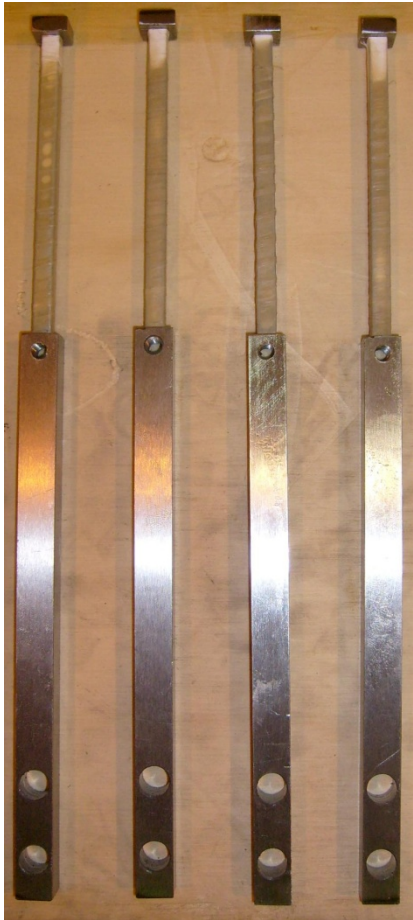
Testing





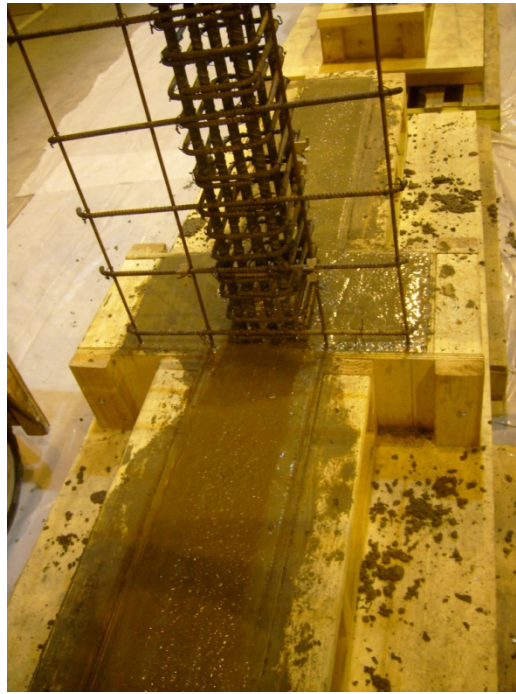
# Shear Devices

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# Casting

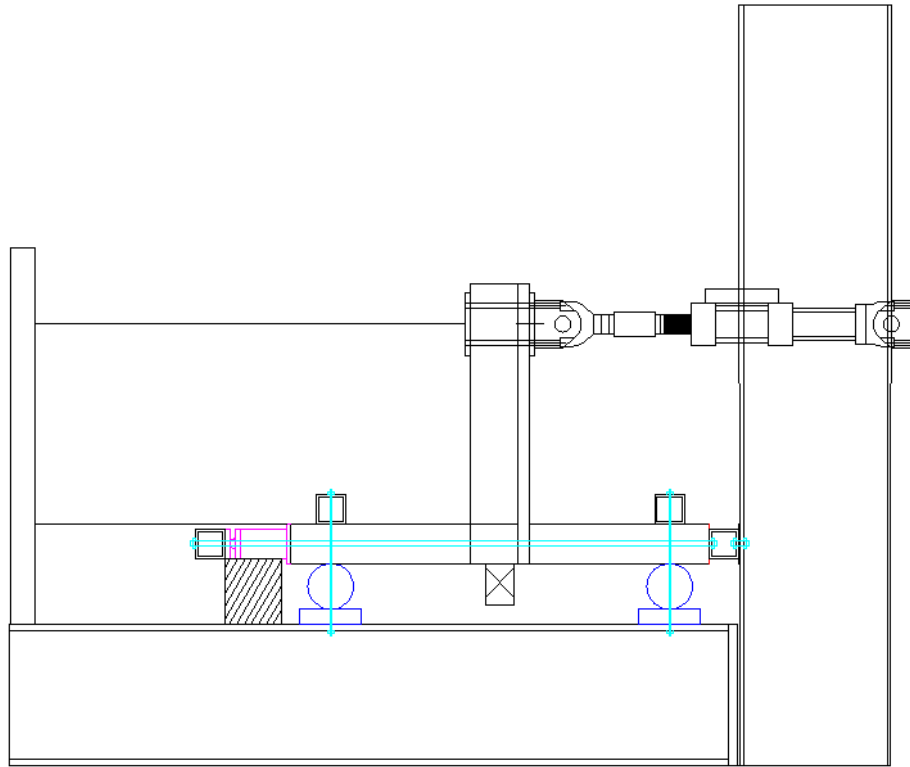
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# Testing

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- Location: Richmond Field Station (Structural Research Laboratory)
- Date: The week of August 18
- Axial Load:  $0.2 A_g f'_c$  (50 kips)  $0.4 A_g f'_c$  (100 kips)
- Beam Loading: Cyclic till failure
- Boundary conditions: Roller and Pin
- Instrumentations:
  - LVDT's (for capturing shear strain)
  - Potentiometers (for capturing beam lateral displacement)

